

Spreading, retraction and sustained oscillations of surfactant-laden lenses

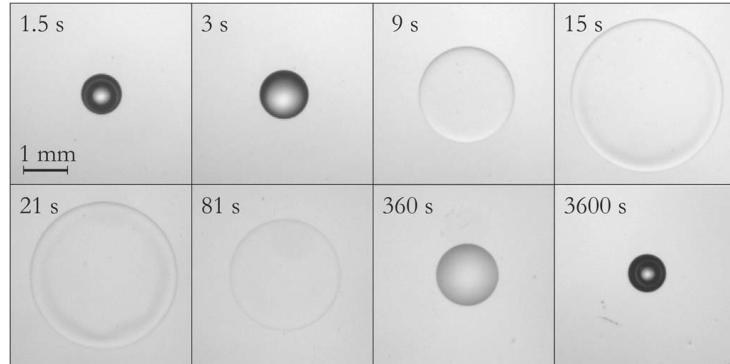
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¹Department of Chemical Engineering

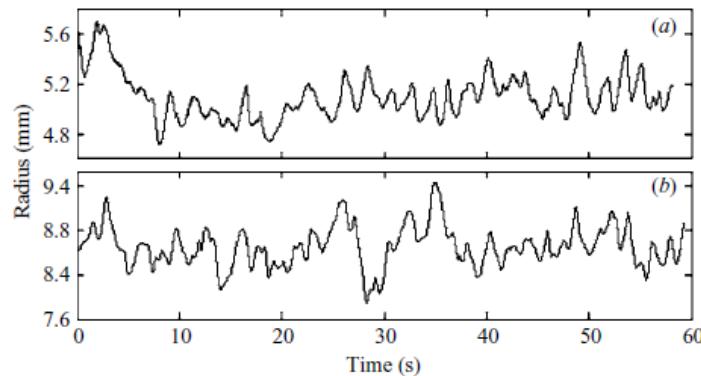
²Department of Mathematics
Imperial College London

Workshop on Surfactant Driven Thin Films Flow
Fields Institute, Toronto, 24 February, 2012

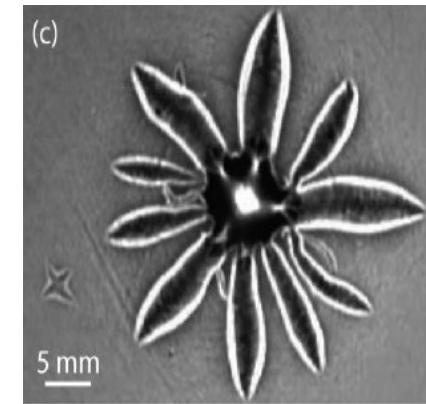
Motivation



Van Nierop et al. PoF 2006



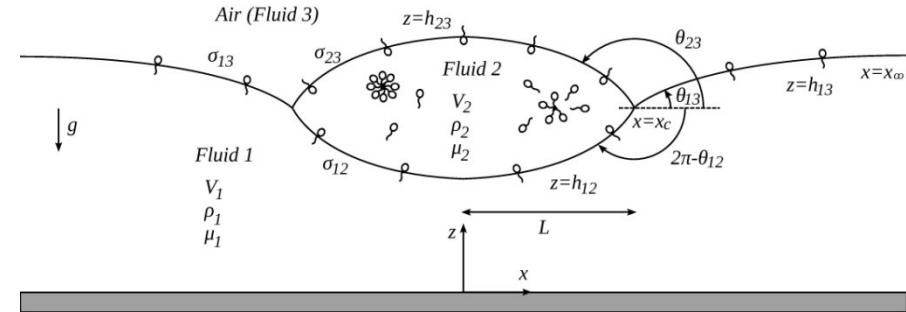
Stocker & Bush JFM 2007



Daniels et al. 2007

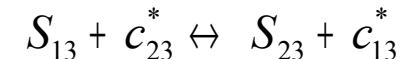
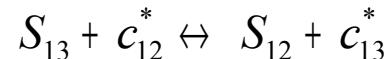
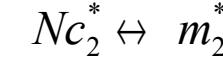
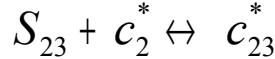
Formulation I

$$\varepsilon = V_2/L^2 \ll 1$$



Surfactant transport and chemical kinetics

S_i = empty space at interface i



Approximations

➤ Lubrication theory

➤ Rapid vertical diffusion

Formulation II

Governing Equations

$$h_{12,t} = - \left(\int_0^{h_{12}} u_1 dz \right)_x$$

$$h_{13,t} = - \left(\int_0^{h_{13}} u_1 dz \right)_x$$

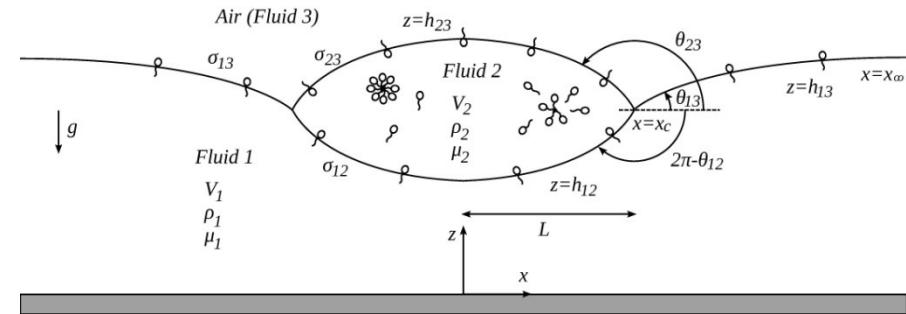
$$h_{23,t} = - \left(\int_0^{h_{12}} u_1 dz + \int_{h_{12}}^{h_{23}} u_2 dz \right)_x$$

where $\int u_i dz = f(h_i, \sigma_i)$

$$c_{2,t} + \frac{c_{2,x}}{h_{23} - h_{12}} \int_{h_{12}}^{h_{23}} u_2 dz = \frac{[(h_{23} - h_{12})c_{2,x}]_x}{(h_{23} - h_{12})Pe_{c2}} - \frac{\beta_{c2c12}}{h_{23} - h_{12}} J_{c2c12} - \frac{\beta_{c2c23}}{h_{23} - h_{12}} J_{c2c23} - J_2$$

$$m_{2,t} + \frac{m_{2,x}}{h_{23} - h_{12}} \int_{h_{12}}^{h_{23}} u_2 dz = \frac{[(h_{23} - h_{12})m_{2,x}]_x}{(h_{23} - h_{12})Pe_{m2}} + J_2$$

J_i = sorption fluxes



Formulation III

$$c_{12,t} + (u_{s,12} c_{12})_x = \frac{c_{12,xx}}{Pe_{12}} + J_{c2c12}$$

$$c_{13,t} + (u_{s,13} c_{13})_x = \frac{c_{13,xx}}{Pe_{13}} + J_{ev13}$$

$$c_{23,t} + (u_{s,23} c_{23})_x = \frac{c_{23,xx}}{Pe_{23}} + J_{c2c23} + J_{ev23}$$

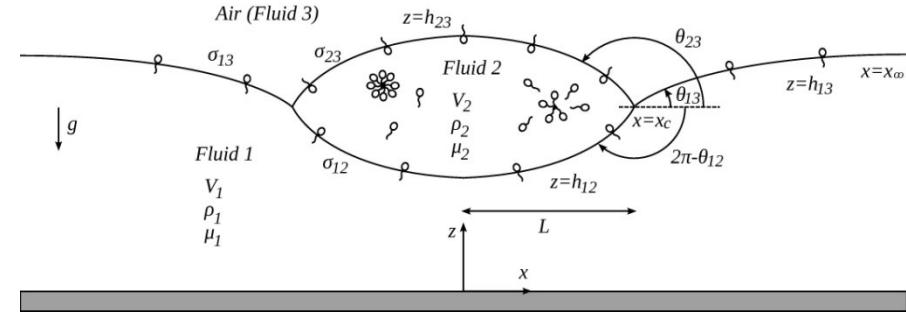
J_i = sorption fluxes

Equation of state

Sheludko 1967

$$\sigma_i = (1 + 1/\Sigma_i) \left(1 + c_i \left((1 + \Sigma_i)^{1/3} - 1 \right) \right)^{-3}$$

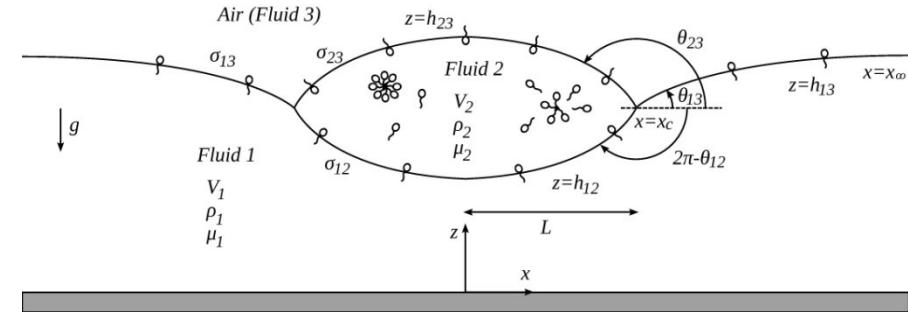
$$\Sigma_i = (\sigma_{io}^* - \sigma_{im}^*) / \sigma_{im}^* \quad \delta_i = \sigma_{im}^* / \sigma_{23m}^* \quad i = 12, 13, 23$$



Formulation IV

Boundary Conditions

Contact line ($x = x_c$)



- $h_{12} = h_{13} = h_{23}$
- Force balance
$$h_{12,x} = h_{23,x} + f(\sigma_i) \quad h_{13,x} = h_{23,x} + g(\sigma_i)$$
- Continuity of pressure
$$F(h_{i,xx}, \sigma_i) = 0$$
- Mass conservation
$$2 \int_0^{x_c} h_{12} dx + 2 \int_{x_c}^{x_\infty} h_{13} dx = V_1 \quad 2 \int_0^{x_c} (h_{23} - h_{12}) dx = V_2$$

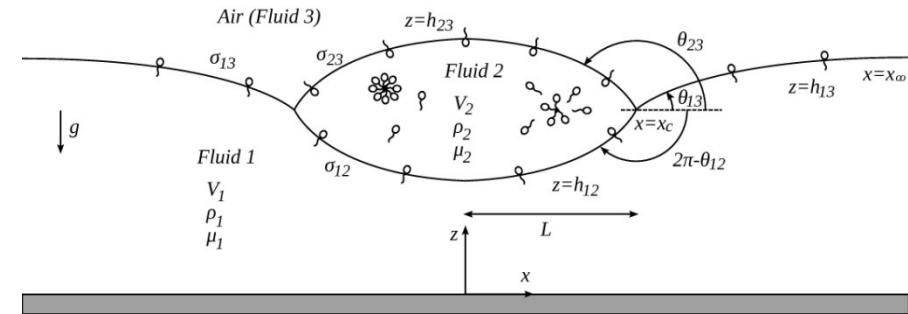
Formulation V

Boundary Conditions

Contact line ($x = x_c$)

$$\left. \frac{c_{23,x}}{Pe_{23}} \right|_{x=x_c} = \beta_{c12c23} J_{c12c23} + \beta_{c13c23} J_{c13c23}$$

$$\left. \frac{c_{12,x}}{Pe_{12}} \right|_{x=x_c} = \beta_{c13c12} J_{c13c12} + J_{c12c23}$$



$$\left. \frac{c_{13,x}}{Pe_{13}} \right|_{x=x_c} = J_{c13c12} + J_{c13c23}$$

Results I

S : spreading parameter

$$S = \sigma_{13} - \sigma_{12} - 1$$

Clean fluid

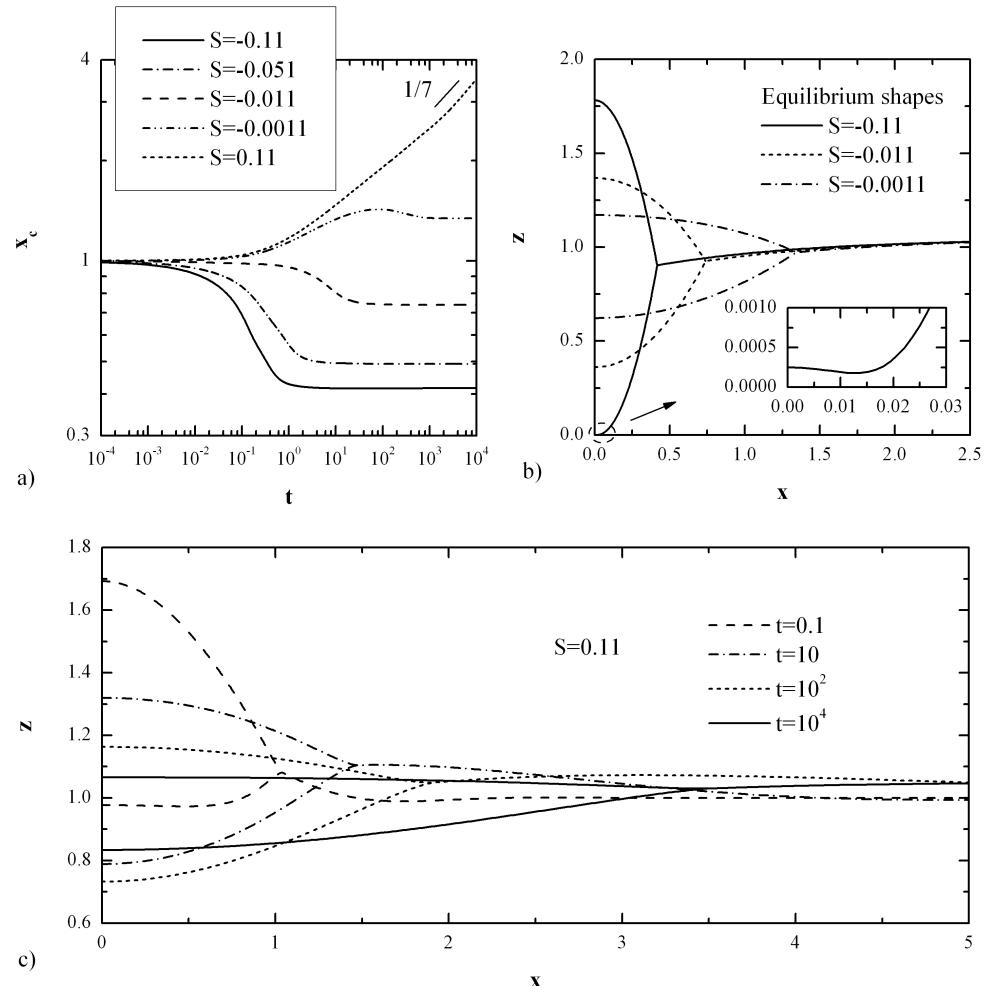
$$\sigma_{12}=1, \rho=1, \mu=1$$

$$\sigma_i = \frac{\sigma_i^* - \sigma_{im}^*}{\sigma_{io}^* - \sigma_{im}^*}$$

$$\rho = \frac{\rho_2^*}{\rho_1^*}$$

$$\mu = \frac{\mu_2^*}{\mu_1^*}$$

Joanny 1987 $\left. \right\} x_c \sim t^{1/7}$
 Fraaije and Cazabat 1989



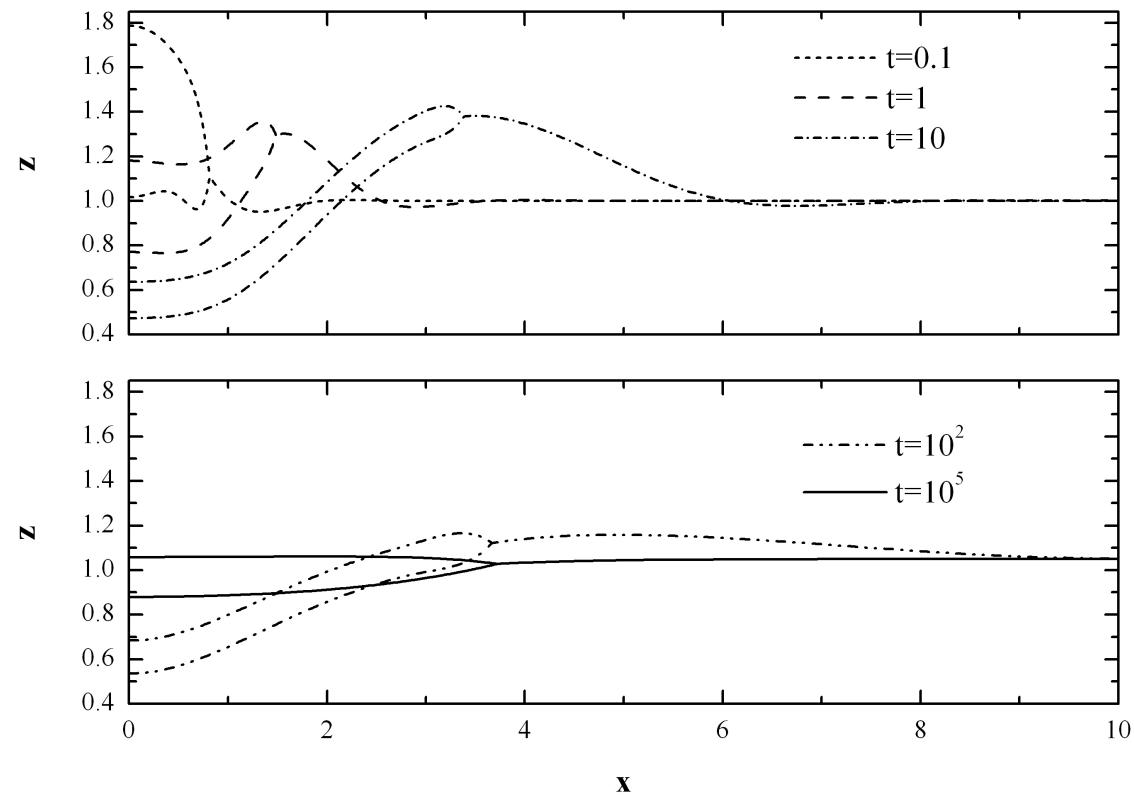
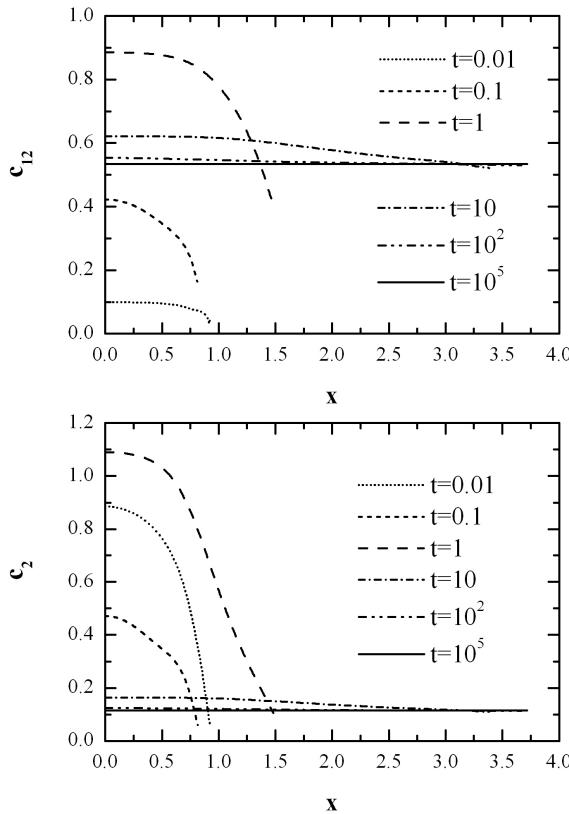
$$M = M^*/(V_2^* c_{cmc}^*) \quad \Sigma_i = (\sigma_{io}^* - \sigma_{im}^*)/\sigma_{im}^* \quad \delta_i = \sigma_{im}^* / \sigma_{23m}^*$$

Results II

Surfactant-laden drop

$M=8$, $\delta_{23}=1.9$, $\delta_{12}=1$,

$\Sigma_i=0.1$, $\rho=\mu=1$

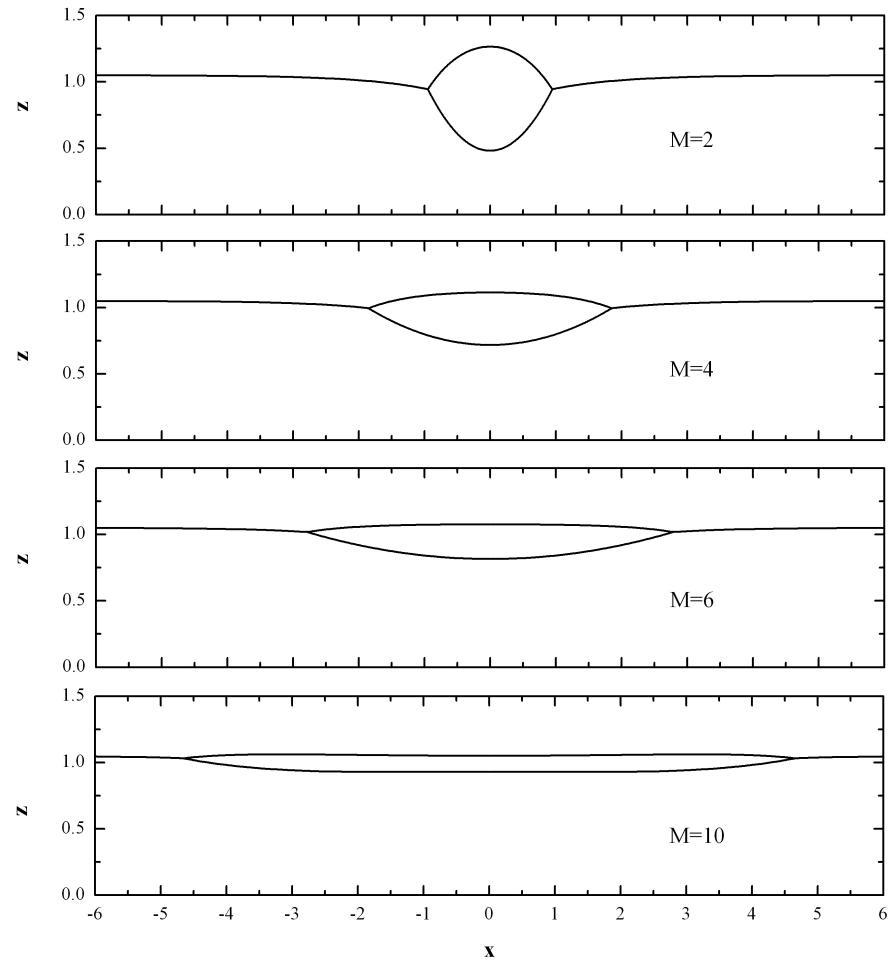
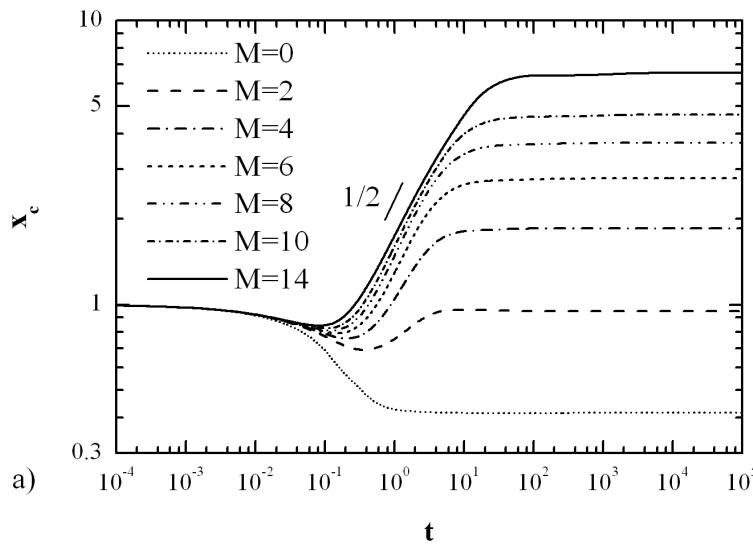


$$M = M^*/(V_2^* c_{cmc}^*) \quad \Sigma_i = (\sigma_{io}^* - \sigma_{im}^*)/\sigma_{im}^* \quad \delta_i = \sigma_{im}^*/\sigma_{23m}^*$$

Results II

Effect of M

$$\delta_{23}=1.9, \delta_{12}=1, \Sigma_i=0.1$$

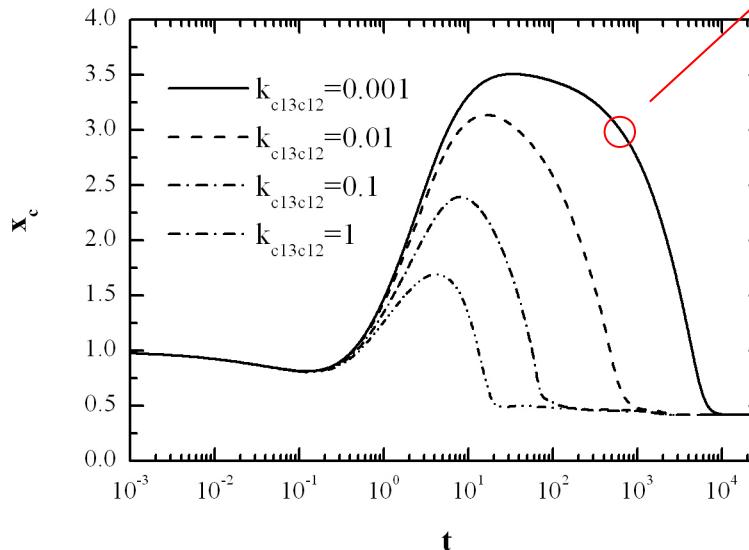


Long time drop shapes, $t=10^5$

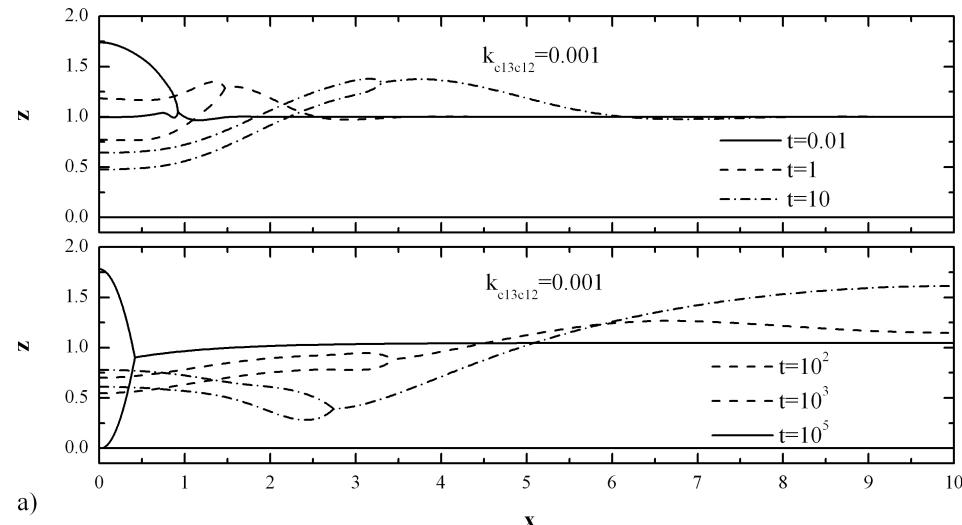
Results IV

Adsorption at the contact line

$$M=8, \delta_{23}=1.9, \delta_{12}=1, \Sigma_i=0.1$$



$$J_{c13c12} = k_{c13c12} [R_{c13c12} c_{13} (1 - c_{12}) - c_{12} (1 - c_{13})]_{x=x_c}$$

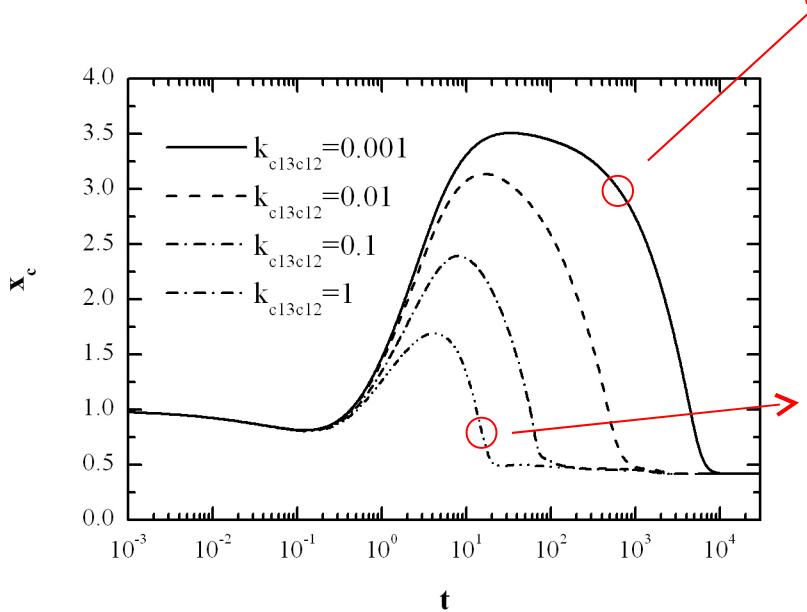


a)

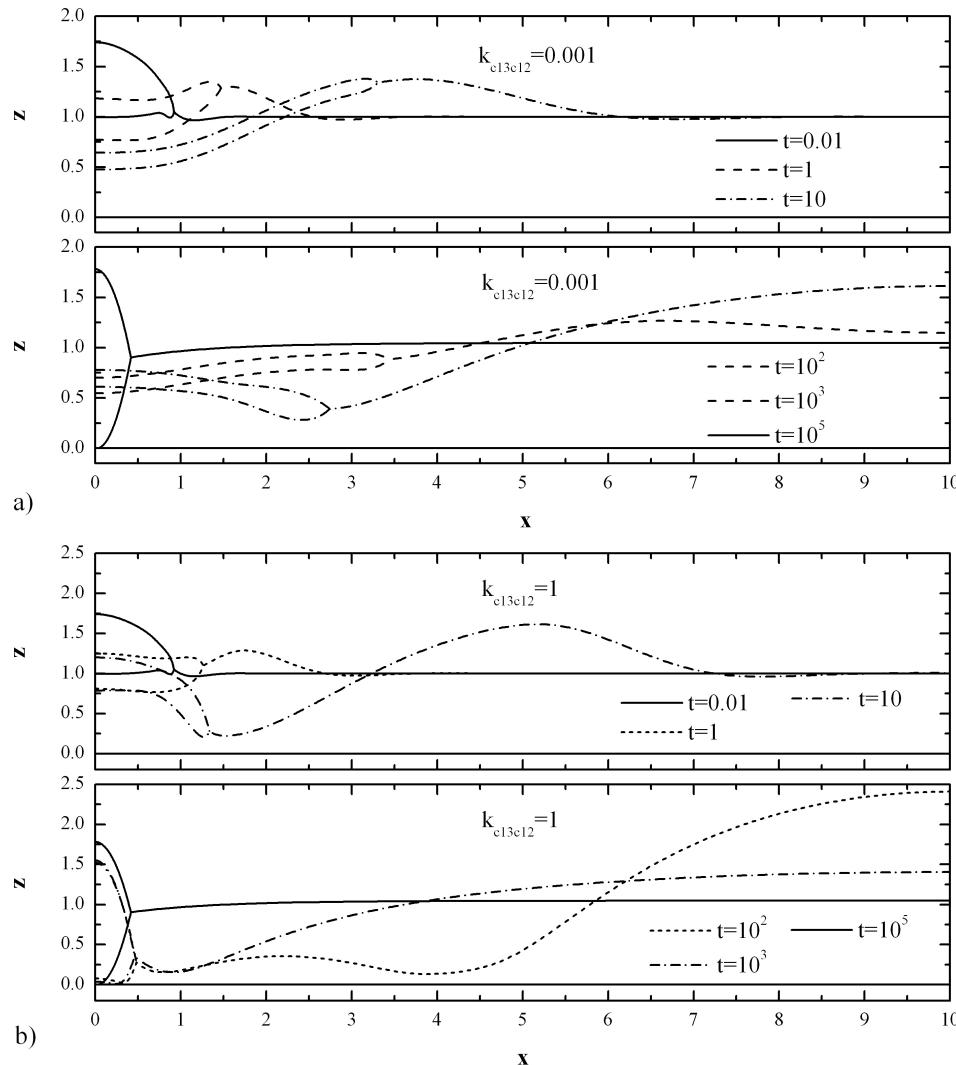
Results IV

Adsorption at the contact line

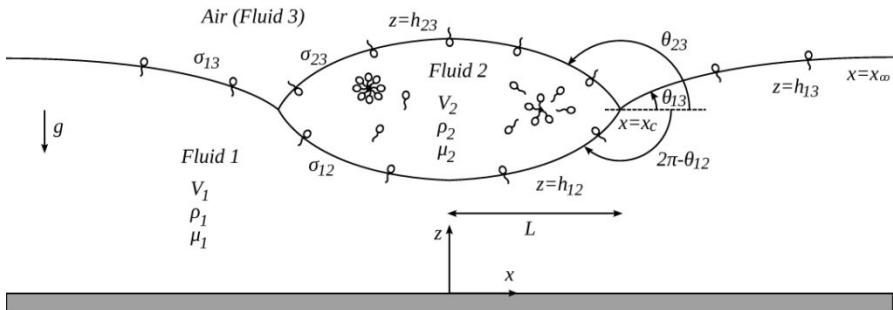
$$M=8, \delta_{23}=1.9, \delta_{12}=1, \Sigma_i=0.1$$



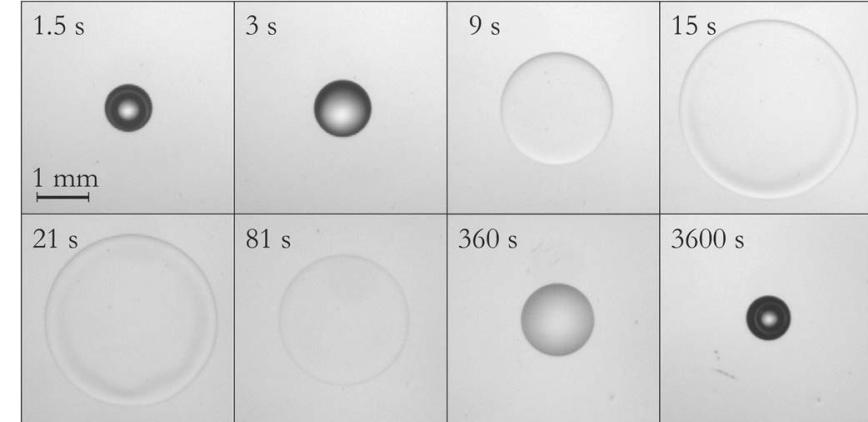
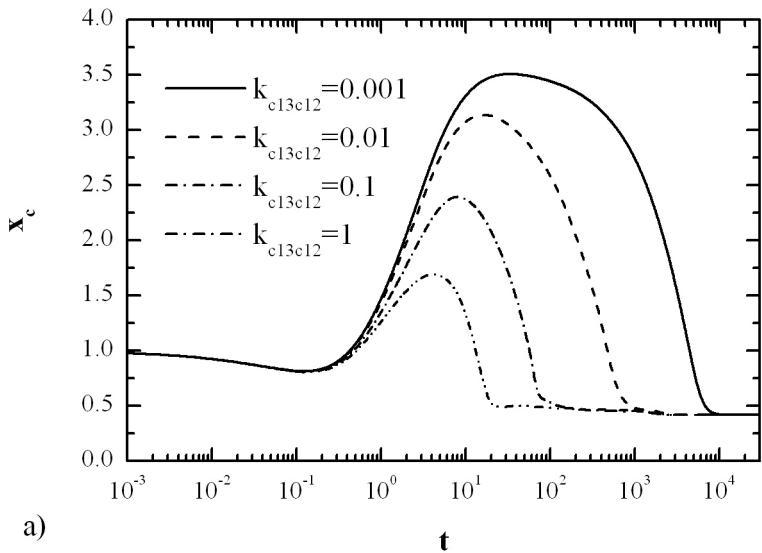
$$J_{c13c12} = k_{c13c12} [R_{c13c12} c_{13} (1 - c_{12}) - c_{12} (1 - c_{13})]_{x=x_c}$$



Results V

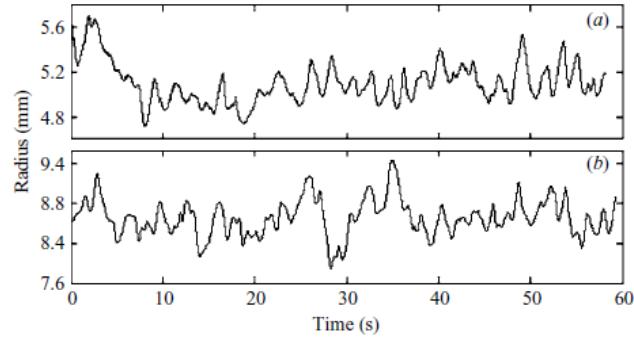


Oil water interface:



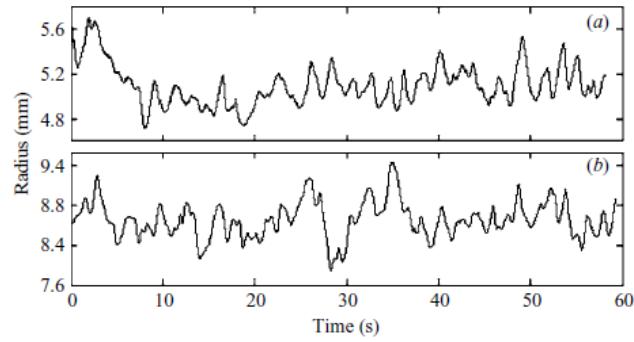
Van Nierop et al. PoF 2006

Results VI

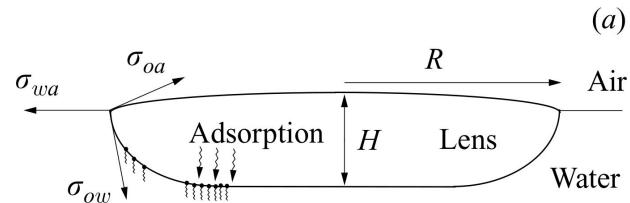


Stocker & Bush JFM 2007

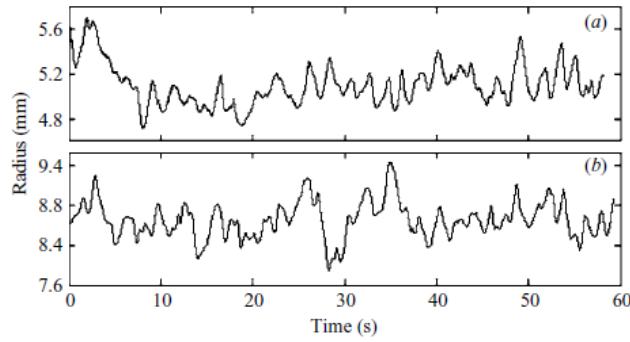
Results VI



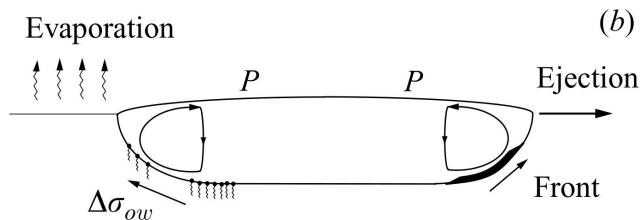
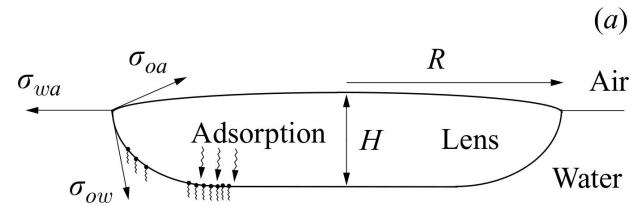
Stocker & Bush JFM 2007



Results VI

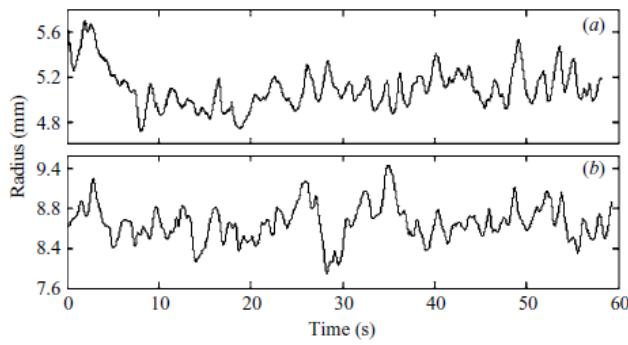


Stocker & Bush JFM 2007

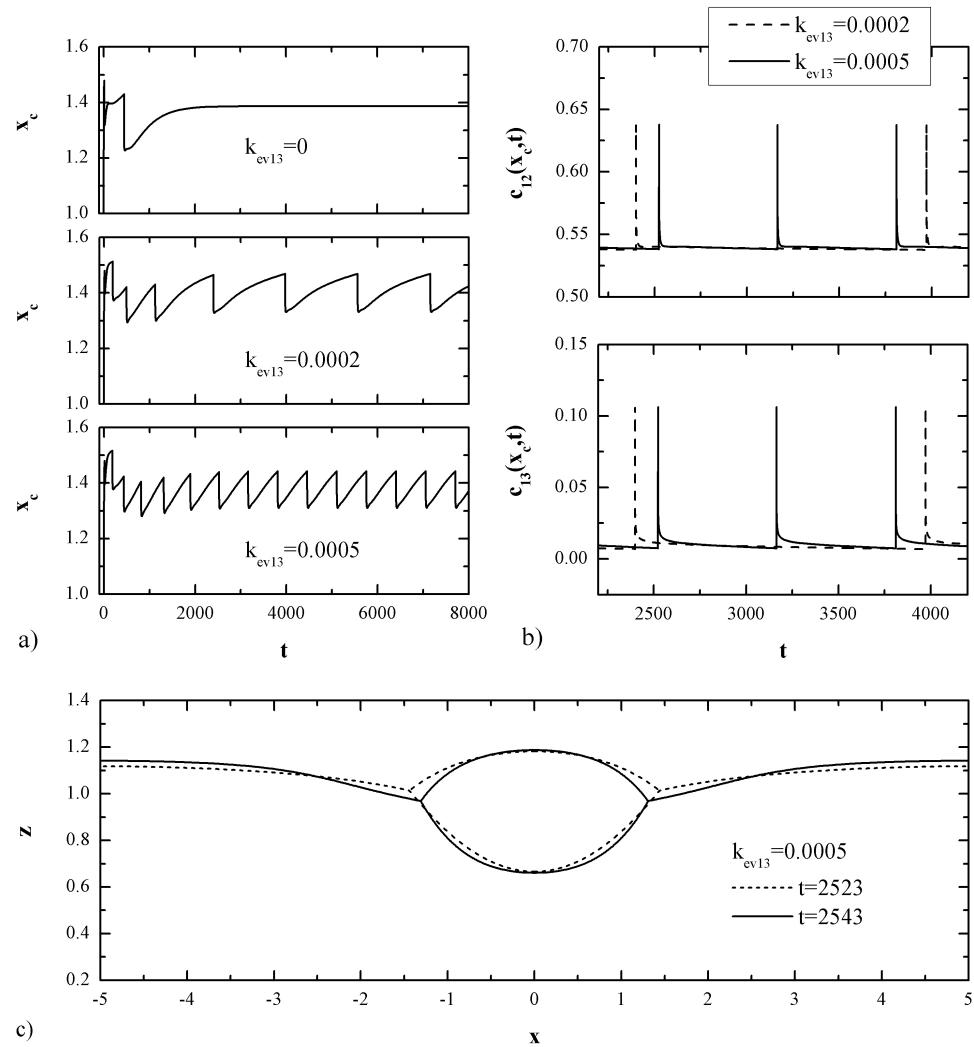
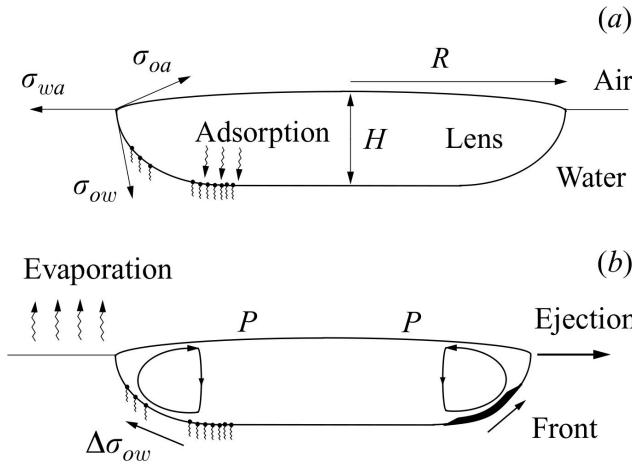


Results VI

k_{ev13} = kinetic parameter for evaporation



Stocker & Bush JFM 2007



$$M = M^*/(V_2^* c_{cmc}^*) \quad \Sigma_i = (\sigma_{io}^* - \sigma_{im}^*)/\sigma_{im}^* \quad \delta_i = \sigma_{im}^*/\sigma_{23m}^*$$

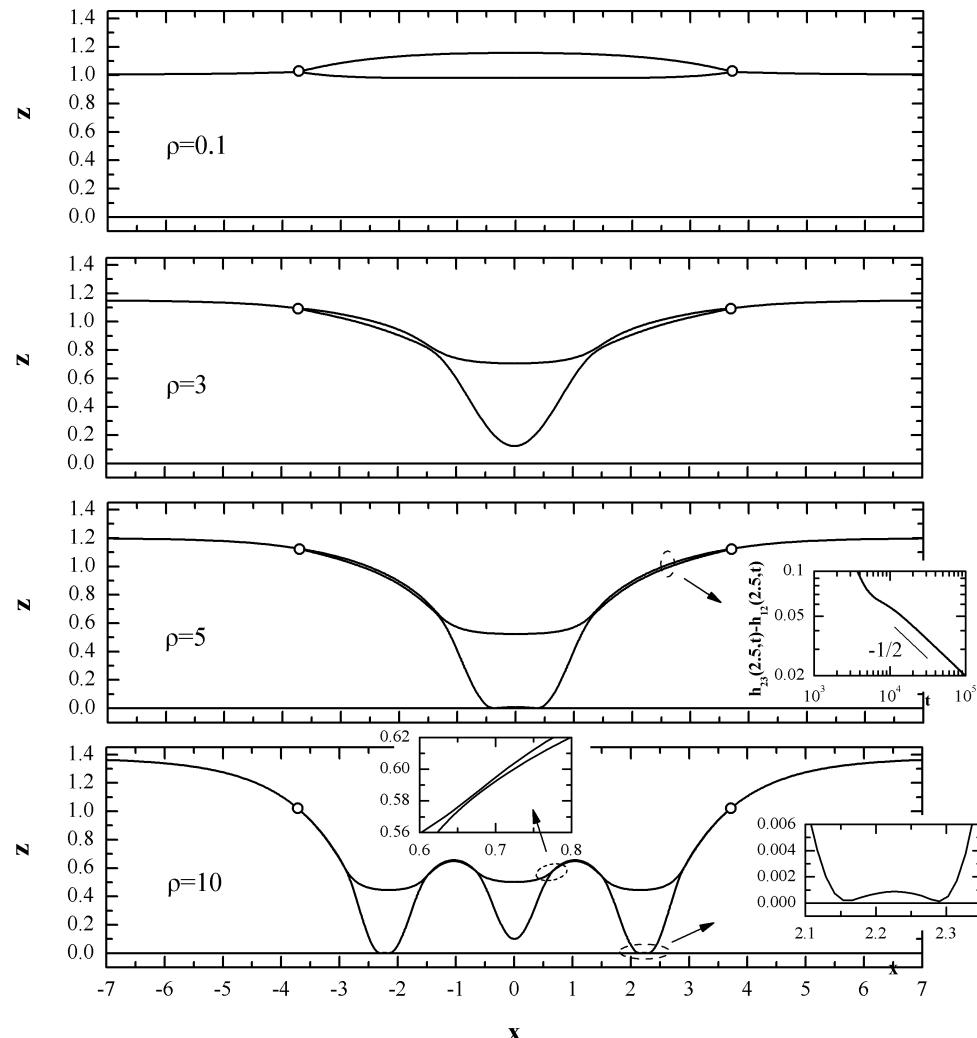
Results VII

Effect of density ratio, ρ

$M=8$, $\delta_{23}=1.9$, $\delta_{12}=1$, $\Sigma_i=0.1$

$$\rho = \frac{\rho_2^*}{\rho_1^*}$$

Long time drop shapes, $t=10^5$



Conclusions

We have studied the spreading of surfactant-laden drops on thin layers of another liquid. The presence of Marangoni stresses gives rise to very rich dynamics which may include:

- Spreading until the drop reaches equilibrium ($S < 0$).
- Continuous spreading ($S > 0$)
- Spreading followed by retraction.
- Self-sustained oscillations.

Thank you for
your attention!